

Solving the 1D Richards Equation by Finite-Difference Approximation

Start with continuity:

$$\frac{\partial \theta}{\partial t} = C(h) \frac{\partial h}{\partial t} = -\frac{\partial q}{\partial z} = -\frac{\partial}{\partial z} \left[-k \frac{\partial h}{\partial z} - k \right] = \frac{\partial}{\partial z} \left[k \frac{\partial h}{\partial z} \right] + \frac{\partial k}{\partial z}$$

For vertical flux (z positive upwards), Darcy gives:

$$C(h) \frac{\partial h}{\partial t} = \frac{\partial}{\partial z} \left[K(h) \left(\frac{\partial h}{\partial z} + 1 \right) \right] = \frac{\partial}{\partial z} \left[k(h) \frac{\partial h}{\partial z} \right] + k'(h) \frac{\partial h}{\partial z}$$

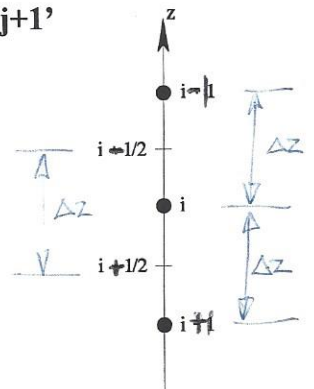
Introduce finite-difference approximation ($\partial \rightarrow \Delta$):

$$C(h) \frac{\Delta h}{\Delta t} = -\frac{\Delta q}{\Delta z}$$

For numerical stability, C and q will be evaluated at the **end of the time step**, i.e., at 'j+1' ("fully implicit method"). Use notation $C_{i,j+1}$ for $C(h_{i,j+1})$ etc.

$$C_{i,j+1} \frac{h_{i,j+1} - h_{i,j}}{\Delta t} = -\frac{q_{i+1/2,j+1} - q_{i-1/2,j+1}}{\Delta z}$$

if $z \rightarrow$ upward.



Substitute Darcy, define $K' = \frac{\partial K}{\partial h}$ (analytically obtained):

$$C_{i,j+1} \frac{h_{i,j+1} - h_{i,j}}{\Delta t} = \frac{K_{i+1/2,j+1} \frac{h_{i+1,j+1} - h_{i,j+1}}{\Delta z} - K_{i-1/2,j+1} \frac{h_{i,j+1} - h_{i-1,j+1}}{\Delta z}}{\Delta z} + K'_{i,j+1} \frac{h_{i+1,j+1} - h_{i-1,j+1}}{2\Delta z}$$

Expand $K_{i+1/2,j+1}$ and $K_{i-1/2,j+1}$:

$$C_{i,j+1} \frac{h_{i,j+1} - h_{i,j}}{\Delta t} = \frac{\frac{K_{i,j+1} + K_{i+1,j+1}}{2} \frac{h_{i+1,j+1} - h_{i,j+1}}{\Delta z} - \frac{K_{i-1,j+1} + K_{i,j+1}}{2} \frac{h_{i,j+1} - h_{i-1,j+1}}{\Delta z}}{\Delta z} + K'_{i,j+1} \frac{h_{i+1,j+1} - h_{i-1,j+1}}{2\Delta z}$$

$\nearrow h_{i-1,j+1}$

Now re-arrange:

$$h_{i,j} \frac{-C_{i,j+1}}{\Delta t} = h_{i-1,j+1} \left(\frac{K_{i-1,j+1} + K_{i,j+1}}{2(\Delta z)^2} - \frac{K'_{i,j+1}}{2\Delta z} \right) +$$

$$h_{i,j+1} \left(-\frac{K_{i,j+1} + K_{i+1,j+1}}{2(\Delta z)^2} - \frac{K_{i-1,j+1} + K_{i,j+1}}{2(\Delta z)^2} - \frac{C_{i,j+1}}{\Delta t} \right) +$$

$$h_{i+1,j+1} \left(\frac{K_{i,j+1} + K_{i+1,j+1}}{2(\Delta z)^2} + \frac{K'_{i,j+1}}{2\Delta z} \right)$$

Defining

$$a_i = \left(\frac{K_{i-1,j+1} + K_{i,j+1}}{2(\Delta z)^2} - \frac{K'_{i,j+1}}{2\Delta z} \right),$$

$$b_i = \left(-\frac{K_{i,j+1} + K_{i+1,j+1}}{2(\Delta z)^2} - \frac{K_{i-1,j+1} + K_{i,j+1}}{2(\Delta z)^2} - \frac{C_{i,j+1}}{\Delta t} \right),$$

$$c_i = \left(\frac{K_{i,j+1} + K_{i+1,j+1}}{2(\Delta z)^2} + \frac{K'_{i,j+1}}{2\Delta z} \right),$$

$f_i = h_{ij} \frac{-C_{ij+1}}{\Delta t} = h_{ij} * d_i$

~~$f_i = h_{ij} \frac{-C_{ij+1}}{\Delta t}$~~

~~$h_{ij} * d_i$~~ , where $d_i = -\frac{C_{ij+1}}{\Delta t}$

we can write the equation for an *internal* node 'i' as follows:

$$a_i h_{i-1,j+1} + b_i h_{i,j+1} + c_i h_{i+1,j+1} = f_i$$

[16]

Thus, for this type of approximation, the h-value at spatial node 'i' at time 'j+1' depends only on the two nearest neighbors, 'i-1' and 'i+1,' as well as on $h_{i,j}$. In matrix notation, we have for a five-node system:

$$\begin{bmatrix} b_1 & c_1 & 0 & 0 & 0 \\ a_2 & b_2 & c_2 & 0 & 0 \\ 0 & a_3 & b_3 & c_3 & 0 \\ 0 & 0 & a_4 & b_4 & c_4 \\ 0 & 0 & 0 & a_5 & b_5 \end{bmatrix} \begin{bmatrix} h_{1,j+1} \\ h_{2,j+1} \\ h_{3,j+1} \\ h_{4,j+1} \\ h_{5,j+1} \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ f_4 \\ f_5 \end{bmatrix}$$



UNKNOWN

Obviously, b_1, c_1, f_1 and a_5, b_5, f_5 have to be obtained from the *boundary conditions* of the particular problem.

And rewrite $\{$ matrix equations for $i=2$ and 4 ;
using [16] side grid

$i=2$:

$$a_2 h_{1j+1} + b_2 h_{2j+1} + c_2 h_{3j+1} = f_2$$

$$\text{or } b_2 h_{2j+1} + c_2 h_{3j+1} = f_2 - a_2 h_{1j+1}$$

known
boundary
conditions.

$i=4$:

$$a_4 h_{3j+1} + b_4 h_{4j+1} = f_4 - c_4 h_{5j+1}$$

Yields.

$$\begin{bmatrix} b_2 & c_2 & 0 \\ a_3 & b_3 & c_3 \\ 0 & a_4 & b_4 \end{bmatrix}
 \begin{bmatrix} h_2 \\ h_3 \\ h_4 \end{bmatrix}_{j+1} = \begin{bmatrix} f_2 - a_2 \overset{\text{known}}{\circlearrowleft} h_{1j+1} \\ f_3 \\ f_4 + c_4 \underset{\text{known}}{\circlearrowright} h_{5j+1} \end{bmatrix} \quad [17]$$

thus if h boundary conditions at both ends
than $[N-2]$ equations and unknowns,

where N is total # of nodes. [Dirichlet boundary condition]

However, alternatively one can define

flux boundary condition, i.e., $q = -k(h) \frac{dh}{dz}$.
 \Rightarrow Neumann b.c

Flux b.c. [Neumann b.c.]

Assign fictitious gridpoints: ^{false} h_0 and h_6 .

	i
x	0
x	1
x	2
x	3
x	4
x	5
x	6

From [16]

$$a_i h_{i-1j+1} + b_i h_{ij+1} + c_i h_{i+1j+1} = d_i h_{ij}$$

$$a_1 h_{0j+1} + b_1 h_{1j+1} + c_1 h_{2j+1} = d_1 h_{1j} \quad i=1$$

$$\vdots$$

$$a_5 h_{4j+1} + b_5 h_{5j+1} + c_5 h_{6j+1} = d_5 h_{5j} \quad i=5$$

$i=1$

[16]

$i=5$

Now 7 unknown's [h_0 through h_6] and 5 equations

Darg equation: for $i=1$

$$q_{1j+1} = -K_{1j+1} \left[\frac{h_{2j+1} - h_{0j+1}}{2\Delta z} + 1 \right]$$

← central difference approx.

$$\frac{q_{1j+1}}{K_{1j+1}} + 1 = - \left(\frac{h_{2j+1} - h_{0j+1}}{2\Delta z} \right)$$

or:

$$h_{0j+1} - h_{2j+1} = 2\Delta z \left[\frac{q_{1j+1}}{K_{1j+1}} + 1 \right] = FLUT$$

(is known from flux b.c.)

$$\Rightarrow \boxed{h_{0j+1} = h_{2j+1} + FLUT} \quad \checkmark$$

Thus, h_0 is determined such that flux through surface is equal to prescribed flux h_c

i.e. Check for $q_1 = 0$ ~~then FLUT = 20z~~

then $h_0 = h_2 + 20z \rightarrow$ yields $q_1 = \phi$ ok.
3

Substitute result in [16] for $i=1$

$$a_1 [h_{2j+1} + \text{FLUT}] + b_1 h_{1j+1} + c_1 h_{2j+1} = d_1 h_{1j}$$

or: $\rightarrow b_1 h_{1j+1} + [a_1 + c_1] h_{2j+1} = d_1 h_{1j} - a_1 * \text{FLUT.}$ [17]

set aside

Similarly for bobbin with $i=5$

$$q_{5j+1} = -K_{5j+1} \left[\frac{h_{6j+1} - h_{4j+1}}{20z} + 1 \right]$$

$$h_{6j+1} - h_{4j+1} = -20z \left[\frac{q_{5j+1}}{K_{5j+1}} + 1 \right] = \text{FLUB} \quad \leftarrow$$

$$\underline{h_{6j+1} = h_{4j+1} + \text{FLUB.}}$$

Substitute in [16] for $i=5$.

$$a_5 h_{4j+1} + b_5 h_{5j+1} + c_5 [h_{4j+1} + \text{FLUB}] = d_5 h_{5j}$$

or $\rightarrow [a_5 + c_5] h_{4j+1} + b_5 h_{5j+1} = d_5 h_{5j} - c_5 \text{FLUB.}$ [18]

set aside

Now new matrix solution

(21)

$$\begin{bmatrix} b_1 & (a_1 + c_1) & 0 & 0 & 0 \\ a_2 & b_2 & c_2 & 0 & 0 \\ 0 & a_3 & b_3 & c_3 & 0 \\ 0 & 0 & a_4 & b_4 & c_4 \\ 0 & 0 & 0 & (a_5 + c_5) & b_5 \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \\ h_3 \\ h_4 \\ h_5 \end{bmatrix} = \begin{bmatrix} d_1 h_1 - a_1 \text{ FLUT} \\ d_2 h_2 \\ d_3 h_3 \\ d_4 h_4 \\ d_5 h_5 - c_5 \text{ FLUB} \end{bmatrix}$$

(false)

but 5 rows

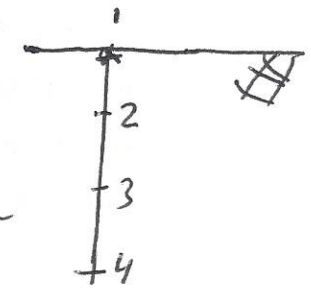
Fictitious grids is convenient way to represent flux bc, but not required. Alternatively, use Taylor series expansion to express h_2 or h_5 from 2 inner nodes and flux b.c. \Rightarrow 3 point - finite difference approx.

See Venuri & Karplus, 1988; page 96.

Expand both h_2 and h_3 around h_1

$$h_2 = h_1 + \left. \frac{dh}{dz} \right|_1 \Delta z + \frac{1}{2} \left. \frac{d^2h}{dz^2} \right|_1 (\Delta z)^2 + \dots$$

$$h_3 = h_1 + \left. \frac{dh}{dz} \right|_1 (2\Delta z) + \frac{1}{2} \left. \frac{d^2h}{dz^2} \right|_1 (2\Delta z)^2 + \dots$$



Subtract

22

Use [19] for both Neumann (flux)
and Dirichlet (head) boundary condition.

Allow [19] for head b.c. :

Set: $b_1 = \cancel{\phi} 1$

$$a_1 + c_1 = \phi$$

$$d_1 h_1 - a_1 \text{ FLUT} = u_{TOP}$$

$$a_2 = \phi$$

Set bottom row:

$$a_5 + c_5 = \phi$$

$$b_5 = 1$$

$$d_5 h_5 - c_5 \text{ FLUB} = u_{BOT}$$

$$c_4 = \phi$$

Now: same matrix as Eq [17]

NEUMANN

Single Matrix for both boundary conditions

$$\begin{bmatrix} b_1 & (a_1+c_1) & 0 & 0 & 0 \\ a_2 & b_2 & c_2 & 0 & 0 \\ 0 & a_3 & b_3 & c_3 & 0 \\ 0 & 0 & a_4 & b_4 & c_4 \\ 0 & 0 & 0 & (a_5+c_5) & b_5 \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \\ h_3 \\ h_4 \\ h_5 \end{bmatrix}_{j+1} = \begin{bmatrix} d_1 h_1 - a_1 \text{ FLUT} \\ f_2 \\ f_3 \\ f_4 \\ d_5 h_5 - c_5 \text{ FLUB} \end{bmatrix}_j$$

DIRICHLET

$$\begin{bmatrix} 1 & \phi & 0 & 0 & 0 \\ 0 & b_2 & c_2 & 0 & 0 \\ 0 & a_3 & b_3 & c_3 & 0 \\ 0 & 0 & a_4 & b_4 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} h_1 \\ h_2 \\ h_3 \\ h_4 \\ h_5 \end{bmatrix}_{j+1} = \begin{bmatrix} u_{\text{TOP}} \\ f_2 - a_2 u_{\text{TOP}} \\ f_3 \\ f_4 - c_4 u_{\text{BOT}} \\ u_{\text{BOT}} \end{bmatrix}_j$$

From:

$$a_i h_{i-1} + b_i h_i + c_i h_{i+1} = f_i \quad [16]$$

$$i = 1, \dots, 5$$

$$\begin{array}{l} a_1 = 0 \\ c_5 = 0 \end{array}$$

Tri diagonal Algorithm

$$\left. \begin{array}{l} Ax = b \\ A = L \cdot U \end{array} \right\}$$

$$L \cdot U \cdot x = b$$

$$A = \begin{bmatrix} b_1 & c_1 & & & \\ a_2 & b_2 & c_2 & & 0 \\ & \ddots & \ddots & \ddots & \\ 0 & & a_n & b_n & \end{bmatrix}$$

$$L \cdot U = A \in$$

solve to get α_i and β_i
of L and U .



$$\alpha_1 * 1 = b_1 \rightarrow \alpha_1 = b_1$$

$$\alpha_1 * \beta_1 = c_1 \rightarrow \beta_1 = c_1 / \alpha_1$$

$$a_2 * \beta_1 + \alpha_2 * 1 = b_2 \rightarrow \alpha_2 = \dots$$

$$a_2 * 0 + \alpha_2 * \beta_2 = c_2 \rightarrow \beta_2 = \dots$$

In General:

$$\alpha_i = b_i \quad \text{and} \quad \beta_i = c_i / \alpha_i$$

$$\alpha_i = b_i - a_i * \beta_{i-1}$$

$$\beta_i = c_i / \alpha_i$$

for $i = 2, \dots, N$.

$$L = \begin{bmatrix} \alpha_1 & & & & \\ a_2 & \alpha_2 & & & \\ & \ddots & \ddots & \ddots & \\ 0 & & a_n & \alpha_n & \end{bmatrix}$$

$$U = \begin{bmatrix} 1 & \beta_1 & & & \\ & 1 & \beta_2 & & \\ & & \ddots & \ddots & \\ & & & \beta_{n-1} & \\ & & & & 1 \end{bmatrix}$$

Tridiagonal or Thomas Algorithm.

Solve $Ax = b$, where $A =$ tri diagonal, and b is known.

Solve for $x!$

Set $A = L.U$ where L : Lower diagonal matrix
 U : Upper diagonal matrix.

$L.Ux = b$ Set $y = Ux$ and Solve $Ly = b$.

Solve for $[y]$ first, then solve for $[x]$.

$$\begin{bmatrix} \alpha_1 & & & & \\ a_2 & \alpha_2 & & & \\ & 0 & \alpha_3 & & \\ & & & \ddots & \\ & & & & a_n \alpha_n \end{bmatrix} \begin{bmatrix} y_1 \\ \vdots \\ y_n \end{bmatrix} = \begin{bmatrix} b_1 \\ \vdots \\ b_n \end{bmatrix}$$

$$\alpha_1 y_1 = b_1 \rightarrow y_1 = \frac{b_1}{\alpha_1}$$

$$a_2 y_1 + \alpha_2 y_2 = b_2 \rightarrow$$

$$y_2 = \frac{b_2 - a_2 y_1}{\alpha_2} \quad \text{or}$$

$$y_i = \frac{b_i - a_i y_{i-1}}{\alpha_i}$$

forward

Then Solve for $Ux = y$

$$\begin{bmatrix} 1 & \beta_1 & & & \\ & 1 & \beta_2 & & \\ & & & \ddots & \\ & & & & \beta_{n-1} \end{bmatrix} \begin{bmatrix} x_1 \\ \vdots \\ x_n \end{bmatrix} = \begin{bmatrix} y_1 \\ \vdots \\ y_n \end{bmatrix}$$

backward substitution:

$$x_n = y_n$$

$$x_{n-1} = y_{n-1} - \beta_{n-1} x_n$$

$$x_i = y_i - \beta_i x_{i+1}$$

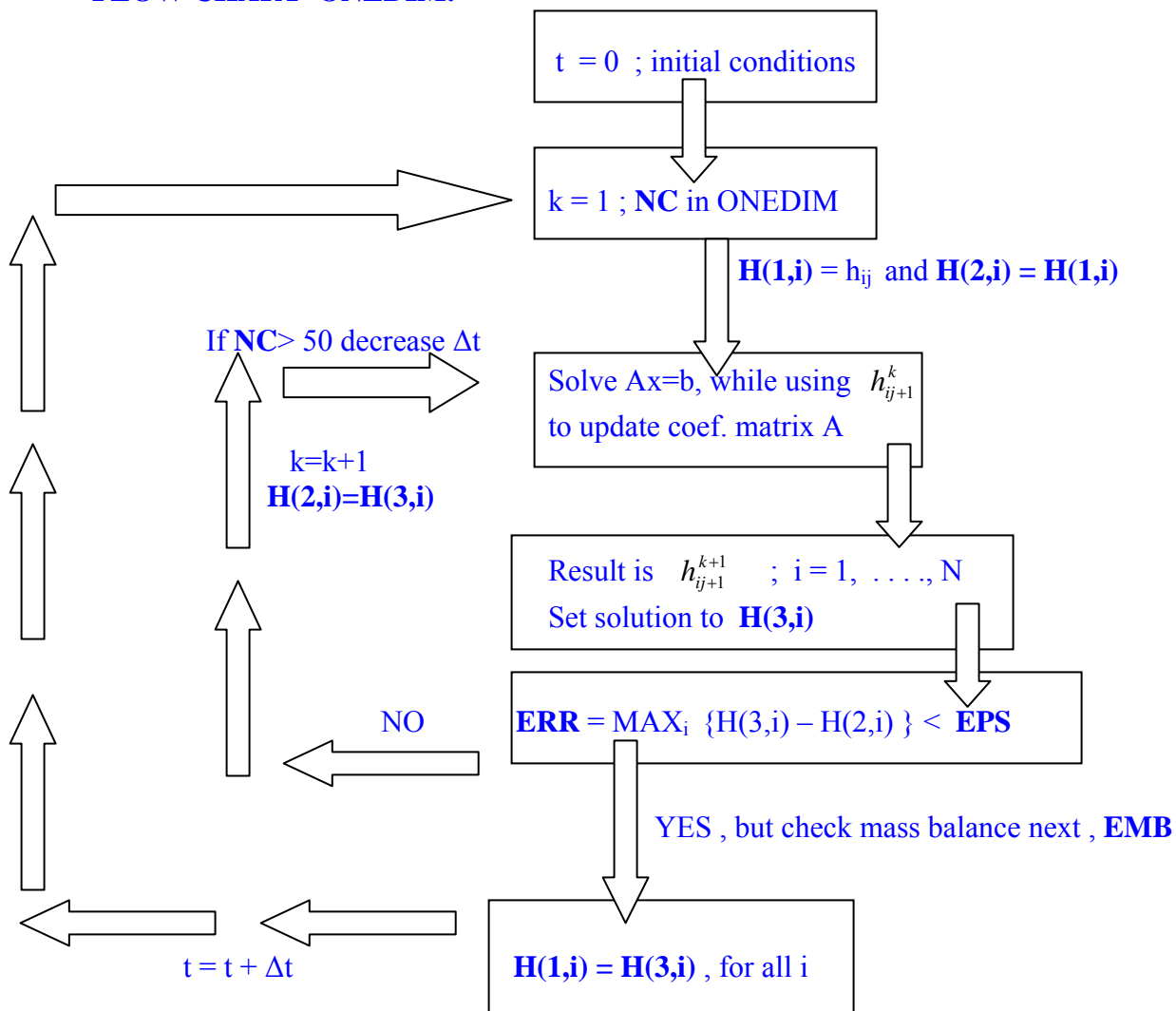
$$i = (n-1), \dots, 1$$

Richards' Equation Flow Charts and Mass Balance Calculations:

In solving Eq. [21], a_i , b_i , and c_i , that include C_i , K_i , as a function of h , are at $(j+1)$ time level. So, although they are in the coefficient matrix, their true values at $(j+1)$ are unknown. How to solve???

At beginning of new time step, $t + \Delta t$, values of K_{ij} and C_{ij} are substituted for K_{ij+1} and C_{ij+1} . The coefficient matrix is solved iteratively, until differences between h_{ij+1}^{k+1} and h_{ij+1}^k are smaller than error criterion, ϵ (EPS) . Realize that superscript (k) denotes the iteration number. This method is called the PICARD ITERATION.

FLOW CHART ONEDIM:



Define relative error between iterations as:

$$ERR = \text{Max}_{i=1,\dots,N} \left| \frac{h_{ij+1}^{(k+1)} - h_{ij+1}^k}{h_{ij+1}^{(k+1)}} \right|$$

If $ERR > \varepsilon$, Re-iterate

If $ERR < \varepsilon$, OK, and h_{ij+1}^{k+1} is the solution. In ONEDIM, $\varepsilon = ERR = 0.001$

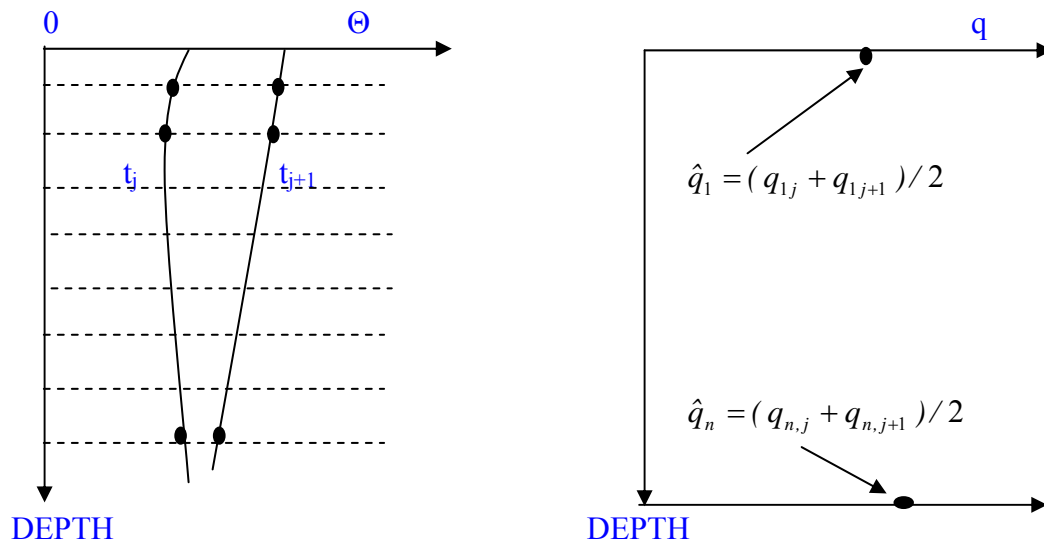
Program ONEDIM limits the nr of iterations NC to 50.

If $NC > 50$, reduce time step by one half, and start over.

So, how about time step size $\Delta t = DT$ (in ONEDIM):

This is done using mass balance calculations:

MASS BALANCE CALCUATIONS in ONEDIM



$\frac{\partial \theta}{\partial t} = -\frac{\partial q}{\partial z}$, for the complete soil domain. That is, between the surface and bottom boundary.

$$d\theta dz = -dq dt \quad \text{or} \quad \int \Delta \theta dz = -\int \Delta q dt$$

$$\Delta \theta = \theta_{i,j+1} - \theta_{i,j} \quad \text{and} \quad \Delta q = q_{in} - q_{out} = \hat{q}_1 - \hat{q}_n$$

$$\text{DELMO} = \int \Delta\theta \, dz = \int_{\text{DEPTH}}^0 (\theta_{i,j+1} - \theta_{i,j}) dz$$

$$\text{DELFLU} = - \int_{t_j}^{t_{j+1}} (q_{in} - q_{out}) dt$$

SO:

Absolute mass balance, $\text{EMB} = \text{DELMO} - \text{DELFLU}$

Relative mass balance, $\text{REMB} = \text{EMB}/\text{DELFLU}$

Now:

If $\text{EMB} > \text{DEL}$ ($\text{DEL} = 0.001$)

Decrease Δt : $\Delta t = 0.5\Delta t$

Start over again, i.e., reject $h_{i,j+1}$ and start re-iterating.

IF $\text{EMB} < (0.1 \times \text{DEL})$

Increase Δt : $\Delta t = 1.5\Delta t$

Now advance in time.

IF $0.1\text{DEL} < \text{EMB} < \text{DEL}$

Advance in time,

But do not change Δt